

HOM damping for future 3-section 200MHz TWCs

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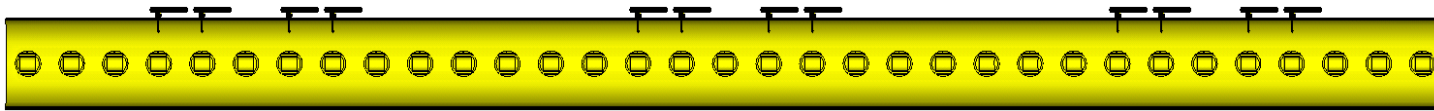


Content

- Damping performance with today's damping scheme
- Effects of adding additional HOM-couplers
 - Increase in impedance of $17\pi/33$ split-mode
- Possible mitigations of $17\pi/33$ split-mode
- Proposals for new HOM-damping schemes
- Conclusions & Outlook

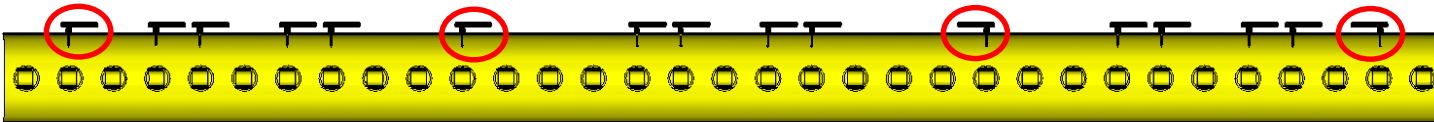
Improvement of present damping scheme

- The present damping scheme is insufficient



3-sections + present HOM damping				
f [MHz]	Q	R/Q [Ω]	R [k Ω]	ρ A
627.7	5600	5.9	33	$17\pi/33$
629.2	445	92	41	$23\pi/33$
630.3	394	137	54	$14\pi/33$

- Effect of additional couplers in E-field maxima of HOMs

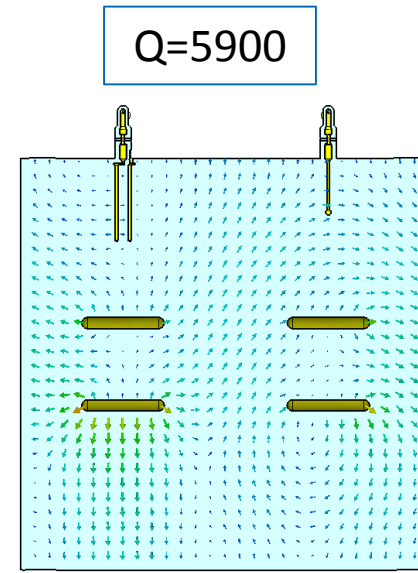
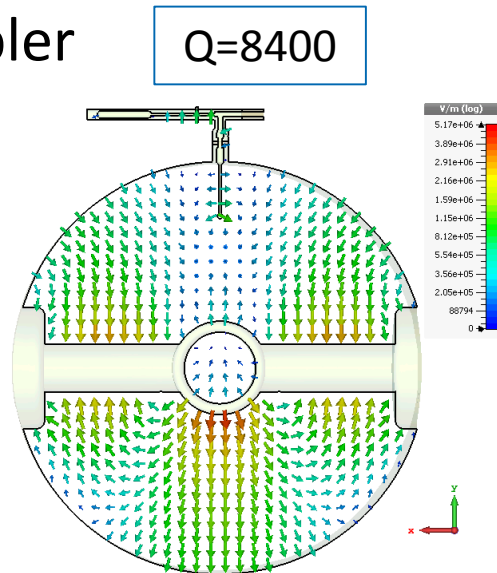
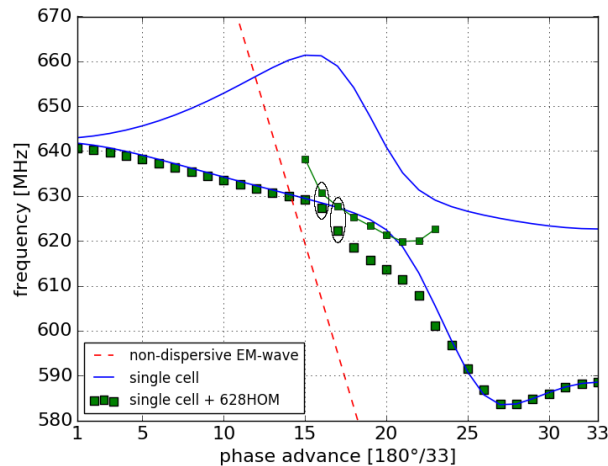


3-sections + additional couplers				
f [MHz]	Q	R/Q [Ω]	R [k Ω]	ρ A
627.7	6952	6.8	47	$17\pi/33$
629.2	296	89	26.1	$23\pi/33$
630.3	224	127	28.5	$14\pi/33$

 Increase in impedance of $17\pi/33$ -mode

Effects of adding HOM-couplers

- Additional modes are created in the dangerous 600MHz cavity passband
- $17\pi/33$ split-mode is particularly detrimental
 - The EM-fields are pushed into the less accessible lower half of the cavity
 - The field strength in the coupler area and the Q are fairly low
- Sufficient damping is very difficult from the top-ports
 - One example: Fork-coupler



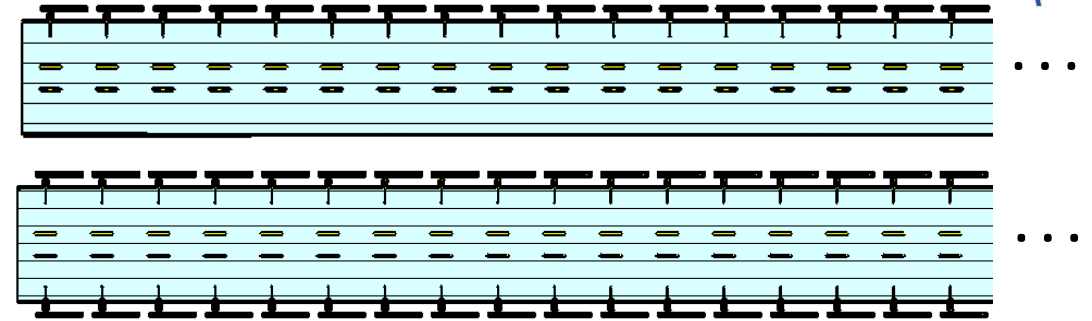
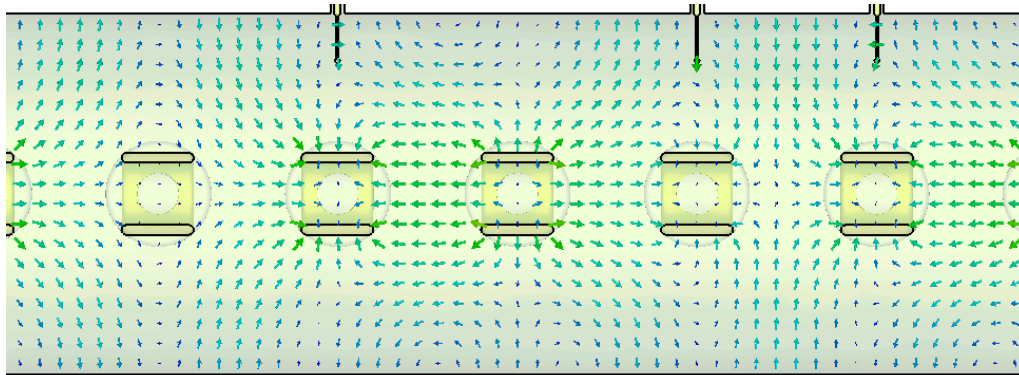
Remember:
 $Q_0=35000$ to $Q_d=3000$
 for $30\pi/44$ -mode

Q is not sufficiently well damped (even in the periodic 2-single-cell approach).

Better understanding of previous efforts



- EM-fields are pushed into lower part of cavity or in-between drift tubes



Courtesy Y. Shashkov

- A sufficient damping solution can not simply be improved by adding additional couplers
 - Especially (already damped) low-Q modes are susceptible to shifts of their EM-fields
 - The damping performance will therefore often even be deteriorated

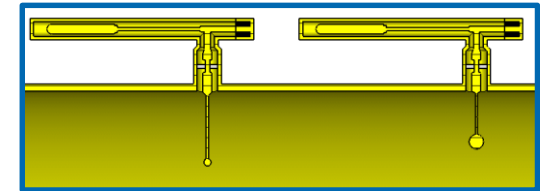
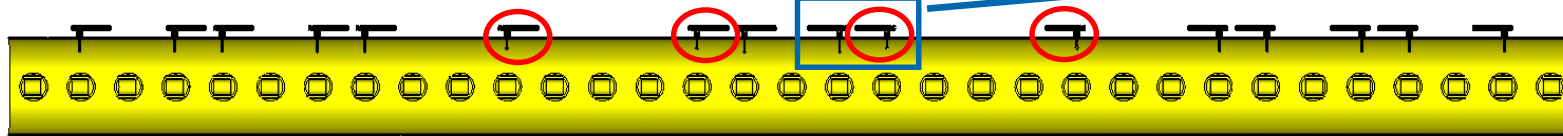


Options for mitigation of $17\pi/33$ -mode

- 1) Avoid $17\pi/33$ -mode impedance to become pronounced
 - Essentially by using less invasive, shorter probes
- 2) Damp $17\pi/33$ -mode in the lower half of the cavity
 - Three proposals will be given

Avoid $17\pi/33$ -mode to become pronounced

- Use shorter probes on HOM-ports where $17\pi/33$ -mode is most susceptible
- Still a sufficient damping performance is necessary
 - Shorter probes on all couplers are not a solution



- This trade-off leads to a balancing of the 3 HOM impedances

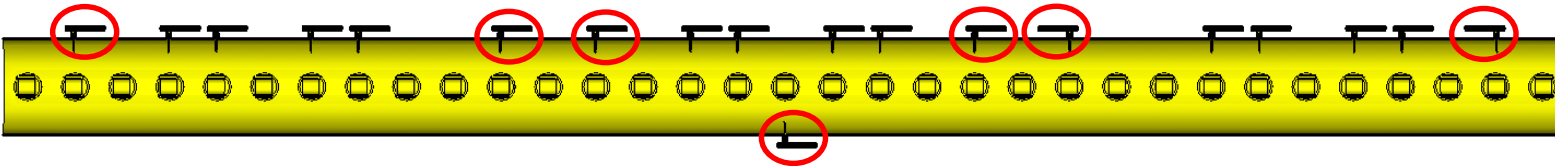
3-sections + HOM trade-off				
f [MHz]	Q	R/Q [Ω]	R [k Ω]	μ A
627.6	5172	5.8	30.0	$17\pi/33$
629.2	325	90	29.3	$23\pi/33$
630.2	245	126	30.5	$14\pi/33$

➔ Impedance is reduced by factor 2.2
(with regard to impedance model)

➔ No room for further damping improvement

Damping via vacuum pumping ports

- All sections have vacuum pumping ports in positions 3, 6, 9
 - Today and in the future not all of them are/ will be used

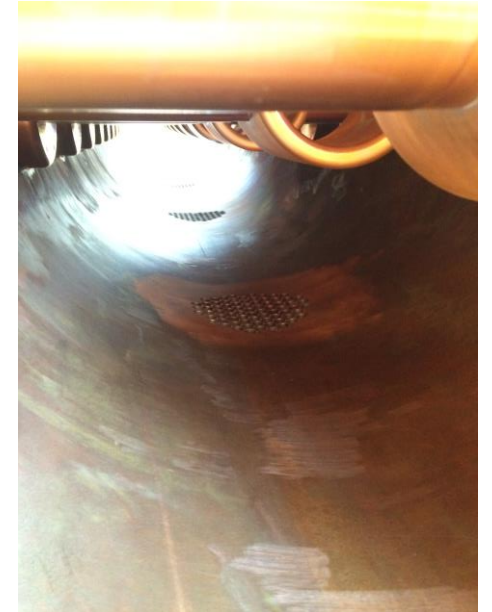


- Sections would most likely need to be machined

3-sections + vacPort17				
f [MHz]	Q	R/Q [Ω]	R [k Ω]	ρA
627.6	3642	3.0	5.5	$17\pi/33$
629.3	262	79	20.8	$23\pi/33$
630.3	194	123	23.9	$14\pi/33$

R/Q is reduced by probe alone

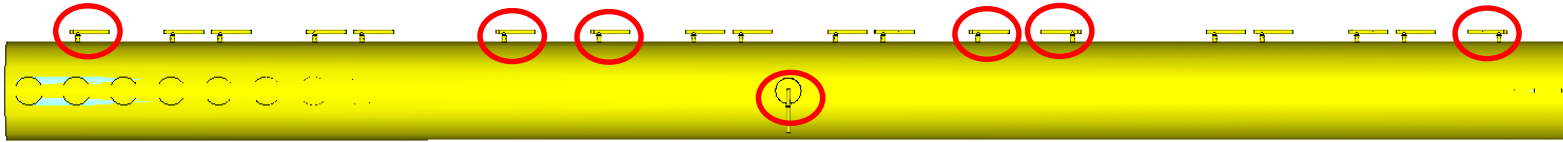
Impedance is reduced by factor 2.8
 (with regard to impedance model)
 Factor 3.1 using two vac-ports



Damping via pedestal



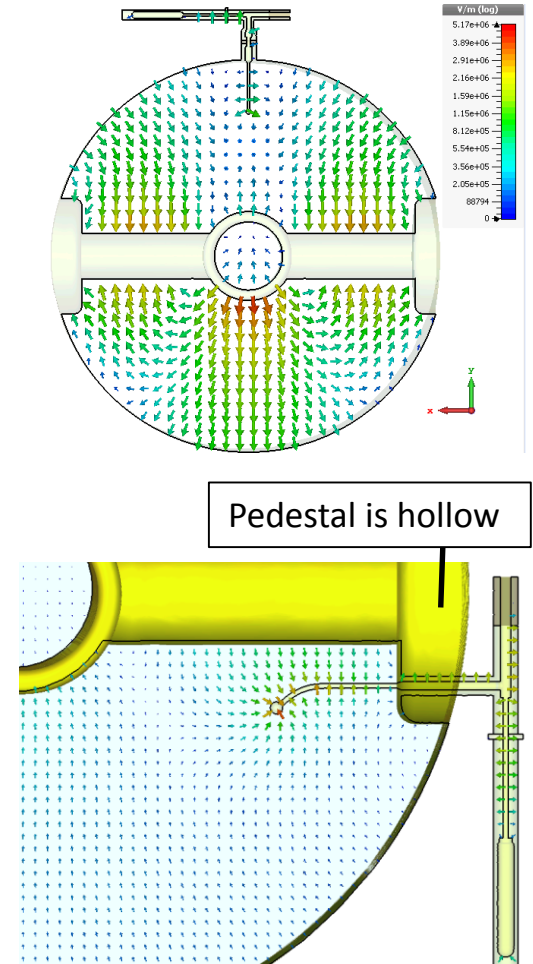
- Only one additional pedestal-coupler is considered
 - New drift-tube would have to be machined & assembled



- Influence on FPB is investigated later in this presentation

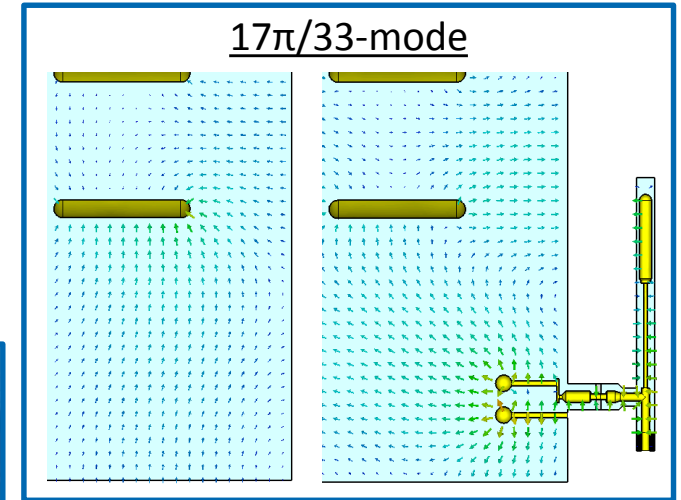
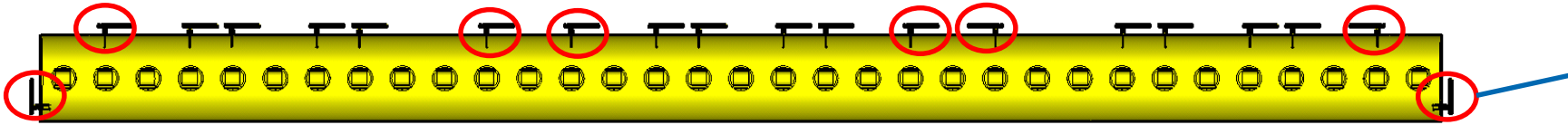
3-sections + pedestal coupler				
f [MHz]	Q	R/Q [Ω]	R [k Ω]	pA
627.6	2070	10.4	21.5	$17\pi/33$
629.3	250	86	21.6	$23\pi/33$
630.3	194	123	24.0	$14\pi/33$

Impedance is reduced by factor 2.8



Damping via endplate HOM-ports

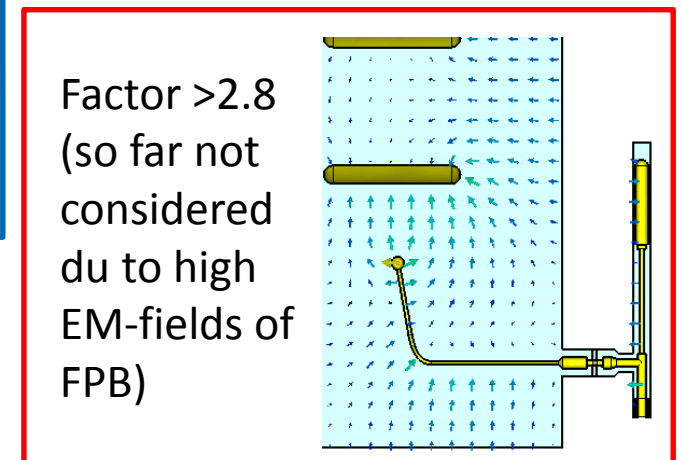
- Ports are currently occupied by 460MHz transverse HOM-couplers
 - Use the lower ports for damping of $17\pi/33$ -mode



- Influence on FPB is investigated on next slide

3-sections + pedestal coupler				
f [MHz]	Q	R/Q [Ω]	R [k Ω]	ρ A
627.6	2550	9.4	23.9	$17\pi/33$
629.5	318	80	25.4	$23\pi/33$
630.4	197	116	22.9	$14\pi/33$

- Damping is also still limited by $17\pi/33$ -mode
- Work ongoing



➔ Impedance is reduced by factor 2.6
(with regard to impedance model)

Influence on the fundamental passband (FPB)



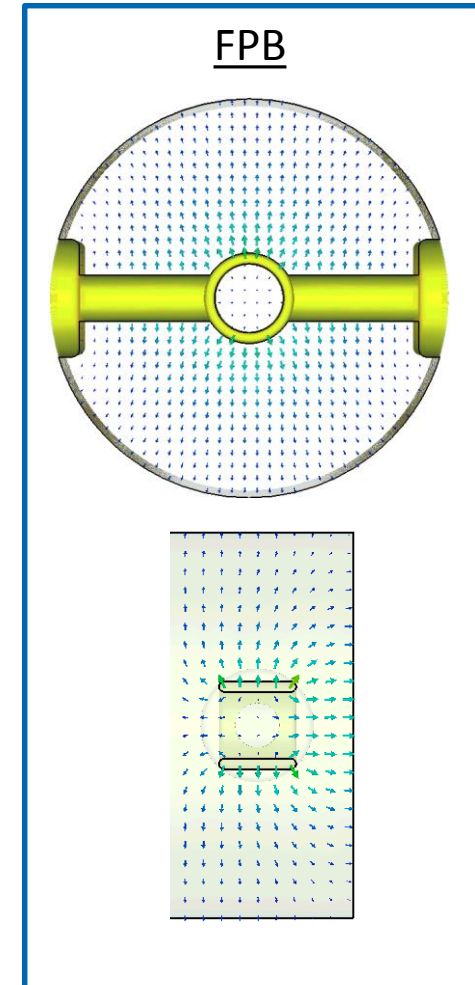
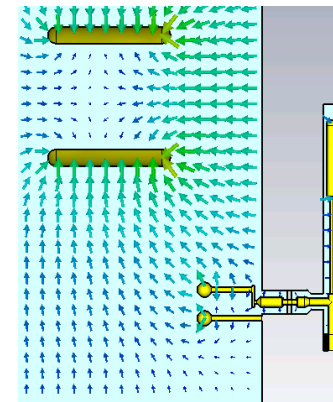
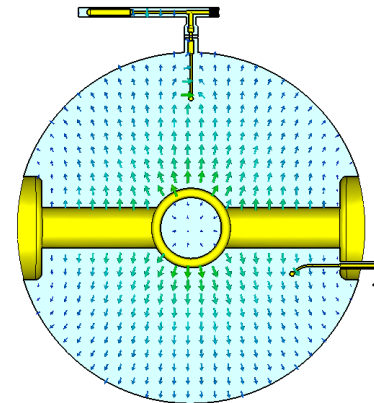
- Vacuum-port-couplers will not have an increased impact on FPB
- Influence of a single pedestal-coupler is negligible
 - Coupling of the probe to the FPB is not strong

	f	Q
sC+628HOM	200.2	22710
sC+628HOM+pedestalHOM	200.2	22706

- Endplate-coupler can couple to FPB

	f	Q
3section+628HOM	200.1	22146
3sec+628HOM+endplateHOM	201.2	22565

➡ More in-depth analysis needed





Conclusions

- Conclusion on endplate-coupler will be given soon
 - Improve damping (on-going simulations, no single-cell approach possible)
 - Investigate impact on 460MHz transverse damping
 - Investigate impact on FPB further
- Mechanical feasibility of vac-port- and pedestal-coupler should be studied (Eric)
- Decision should be made if a slightly less damping would be preferred over cavity machining